

October 12, 2016

Mr. Brian Hocutt
South Mississippi Electric Power Association
P.O. Box 15849
Hattiesburg, MS 39402

Re: CCR Surface Impoundments Initial Inflow Design Flood Control System Plan
R.D. Morrow, Sr. Generating Station
Purvis, Lamar County, Mississippi

Dear Mr. Hocutt:

South Mississippi Electric Power Association (SMEPA) retained Environmental Management Services, Inc. (EMS) to develop an “Initial Inflow Design Flood Control System Plan” (Plan) for the R.D. Morrow, Sr. Generating Station Emergency Scrubber Surge Pond and Scrubber Supply Pond (surface impoundments) located as shown on Figure 1 in Attachment 1 to this Plan. The purpose of this Plan is to ensure that the design of the surface impoundments is sufficient to perform as designed in the case of maximum operating conditions and the appropriate storm event chosen on the basis of the Hazard Classification for the impoundments per Coal Combustion Residuals (CCR) regulations found in 40 CFR Part 257.82.

Site Information

The R.D. Morrow, Sr. Generating Station is located near Purvis in Lamar County, Mississippi just north of Old Okahola School (Okahola) Road. The subject surface impoundments are located just south of the main power block (see Figure 2, Attachment 1) and are located such that discharges or overflows would be conveyed by overflow piping to the Coal Pile Runoff Collection Area immediately down gradient (to the south) from the CCR impoundments. Discharge or overflow from the Coal Pile Runoff Collection Area is conveyed via culvert to Pond 4A which is separated from the Coal Pile Runoff Collection Area by a large railroad spur embankment. The railroad spur is owned by SMEPA and serves to allow storage/routing of rail cars used to deliver coal to the facility. Downstream of Pond 4A is Okahola Road which is a county-maintained paved public road. Excess water from Pond 4A is routed via culvert underneath Okahola Road to the Cooling Tower Blowdown Pond, from where it is eventually discharged under the provisions of a NPDES permit.

Regulatory Background

Regulated surface impoundments that are used to contain and store CCR must meet the following capacity requirements as set forth in 40 CFR Part 257:

§ 257.82 – Hydrologic and hydraulic capacity requirements for CCR surface impoundments.

(a) The owner or operator of an existing or new CCR surface impoundment or any lateral expansion of a CCR surface impoundment must design, construct, operate, and maintain an inflow design flood control system as specified in paragraphs (a)(1) and (2) of this section.

(1) The inflow design flood control system must adequately manage flow into the CCR unit during and following the peak discharge of the inflow design flood specified in paragraph (a)(3) of this section.

(2) The inflow design flood control system must adequately manage flow from the CCR unit to collect and control the peak discharge resulting from the inflow design flood specified in paragraph (a)(3) of this section.

(3) The inflow design flood is:

(i) For a high hazard potential CCR surface impoundment, as determined under § 257.73(a)(2) or § 257.74(a)(2), the probable maximum flood;

(ii) For a significant hazard potential CCR surface impoundment, as determined under § 257.73(a)(2) or § 257.74(a)(2), the 1,000-year flood;

(iii) For a low hazard potential CCR surface impoundment, as determined under § 257.73(a)(2) or § 257.74(a)(2), the 100-year flood; or

(iv) For an incised CCR surface impoundment, the 25-year flood.

The hazard potential classification for a dam (i.e., impoundment) is intended to rank dams in terms of potential losses to downstream interests if the dam should fail for any reason. The classification is based on the incremental adverse consequences (pre vs. post event) of failure or mis-operation of the dam, and has no relationship to the current structural integrity, operational status, flood routing capability, or safety condition of the dam or its appurtenances. The hazard potential classification is based on potential adverse impacts/losses in four categories: environmental, infrastructure, economic, and/or human life. As detailed in the “Hazard Potential Classification Assessment” performed by EMS in October 2016, the impoundments are both classified as Low Hazard Potential. As such, the storm event that must be used for design inflow is the 100-year flood.

(b) Discharge from the CCR unit must be handled in accordance with the surface water requirements under § 257.3-3.

Any discharges from the Emergency Scrubber Surge Pond or the Scrubber Supply Pond are routed through various collection areas prior to introduction to the Cooling Tower Blowdown Pond. The discharge from the Cooling Tower Blowdown Pond is regulated under an NPDES permit and is sampled and reported accordingly.

(c) Inflow design flood control system plan –

(1) Content of the plan. The owner or operator must prepare initial and periodic inflow design flood control system plans for the CCR unit according to the timeframes specified in paragraphs (c)(3) and (4) of this section. These plans must document how the inflow design flood control system has been designed and constructed to meet the requirements of this section. Each plan must be supported by appropriate engineering calculations. The owner or operator of the CCR unit has completed the inflow design flood control system plan when the plan has been placed in the facility's operating record as required by § 257.105(g)(4).

(2) Amendment of the plan. The owner or operator of the CCR unit may amend the written inflow design flood control system plan at any time provided the revised plan is placed in the facility's operating record as required by § 257.105(g)(4). The owner or operator must amend the written inflow design flood control system plan whenever there is a change in conditions that would substantially affect the written plan in effect.

(3) Timeframes for preparing the initial plan – (i) Existing CCR surface impoundments. The owner or operator of the CCR unit must prepare the initial inflow design flood control system plan no later than October 17, 2016.

(ii) New CCR surface impoundments and any lateral expansion of a CCR surface impoundment. The owner or operator must prepare the initial inflow design flood control system plan no later than the date of initial receipt of CCR in the CCR unit.

(4) Frequency for revising the plan. The owner or operator must prepare periodic inflow design flood control system plans required by paragraph (c)(1) of this section every five years. The date of completing the initial plan is the basis for establishing the deadline to complete the first periodic plan. The owner or operator may complete any required plan prior to the required deadline provided the owner or operator places the completed plan into the facility's operating record within a reasonable amount of time. In all cases, the deadline for completing a subsequent plan is based on the date of completing the previous plan. For purposes of this paragraph (c)(4), the owner or operator has completed an inflow design flood control system plan when the plan has been placed in the facility's operating record as required by § 257.105(g)(4).

(5) *The owner or operator must obtain a certification from a qualified professional engineer stating that the initial and periodic inflow design flood control system plans meet the requirements of this section.*

(d) *The owner or operator of the CCR unit must comply with the recordkeeping requirements specified in § 257.105(g), the notification requirements specified in § 257.106(g), and the internet requirements specified in § 257.107(g).*

The following narrative and supporting figures and calculations constitute the ***Initial Inflow Design Flood Control System Plan*** and have been developed to address the requirements as stated in the regulatory reference above.

Emergency Scrubber Surge Pond

The Emergency Scrubber Surge Pond is a small impoundment used to capture overflow from the thickener unit. The pond has a surface area of 18,600 sq. ft. (0.43 acres) at the normal pool elevation of 264 feet, and has an approximate capacity of 728,000 gallons (2.23 acre-feet). Freeboard at normal pool is 2 feet with the crest of the impoundment at an elevation of approximately 267 feet. Due to the design of the pond and surrounding topography, very little run-on is directed into the impoundment. Normal operational flow from the thickener and rain water falling directly on the impoundment and immediate surroundings constitute the only inflows to the pond during storm events. The average daily operational overflow from the thickener unit to the Emergency Scrubber Surge Pond is 376 gallons per minute (gpm). Calculations for this ponds behavior during the 100-year storm event for this locality are included in Attachment 2 to this correspondence.

Scrubber Supply Pond

The Scrubber Supply Pond is a small impoundment used for supplying water to the facility scrubber system. The pond has a surface area of approximately 45,400 sq. ft. (1.04 acres) at the normal pool elevation of 264 feet, and has an approximate capacity of 3,200,500 gallons (9.82 acre-feet). Freeboard at normal pool is 3 feet with the crest of the impoundment at an elevation of approximately 267 feet. Due to the design of the pond and surrounding topography, very little run-on is directed into the impoundment. Normal operational flow and rain water falling directly on the impoundment and immediate surroundings constitute the only inflows to the pond during storm events. The average daily operational input to the pond is 130.1 gpm from plant drains and 376.1 gpm from the thickener unit overflow (via the emergency scrubber surge pond). Calculations for this ponds behavior during the 100-year storm event for this locality are included in Attachment 2.

Results

The hydrologic and hydraulic model included in Attachment 2 has been developed based on the current configuration and piping arrangement observed at the facility in October, 2016. Operational assumptions have been made in order to create the model, and a conservative case has been chosen to demonstrate that the impoundments and hydraulic design can perform adequately during a 100-year, 24-hour storm event. This model assumes that no operational flows are entering or exiting the pond, which is a conservative assumption. If the facility is operating, impoundment withdrawals would be slightly greater than operational inputs and would therefore result in a net reduction in fluid volume in the system without makeup input.

The inputs to the model include: the 100-year, 24-hour storm event (design storm) for the plant area which enters the Scrubber Supply Pond via a sump pump arrangement through a 12-inch diameter HDPE pipe, and the design storm for the Emergency Scrubber Surge Pond and the Scrubber Supply Pond. Based on these inputs, both impoundments are designed and constructed to operate with sufficient freeboard to prevent overtopping their dams. Additional safeguards are in place for preventing dam overtopping including a 6-inch diameter high-level gravity overflow and a 6-inch diameter hose in place to serve as discharge piping for a portable pump should the need arise. The inflow flood control system to the CCR impoundments at this facility is adequate and will preserve the structural integrity of the impoundments during the design case.

Certification

I hereby certify, as a Professional Engineer in the State of Mississippi, that the information in this document was assembled under my direct personal charge. This report is not intended or represented to be suitable for reuse by South Mississippi Electric Power Association or others without specific verification or adaptation by the Engineer. This Inflow Design Flood Control System Plan was developed in accordance with the requirements of 40 CFR Part 257 §82.



Christopher Taylor Johnson, P.E. MS #15761

Qualified Professional Engineer

Date: 10/12/2016

Should you have any questions regarding this document please contact the undersigned at (601) 544-3674. We appreciate the opportunity to assist SMEPA in achieving compliance with CCR regulations.

Sincerely,

Environmental Management Services, Inc.



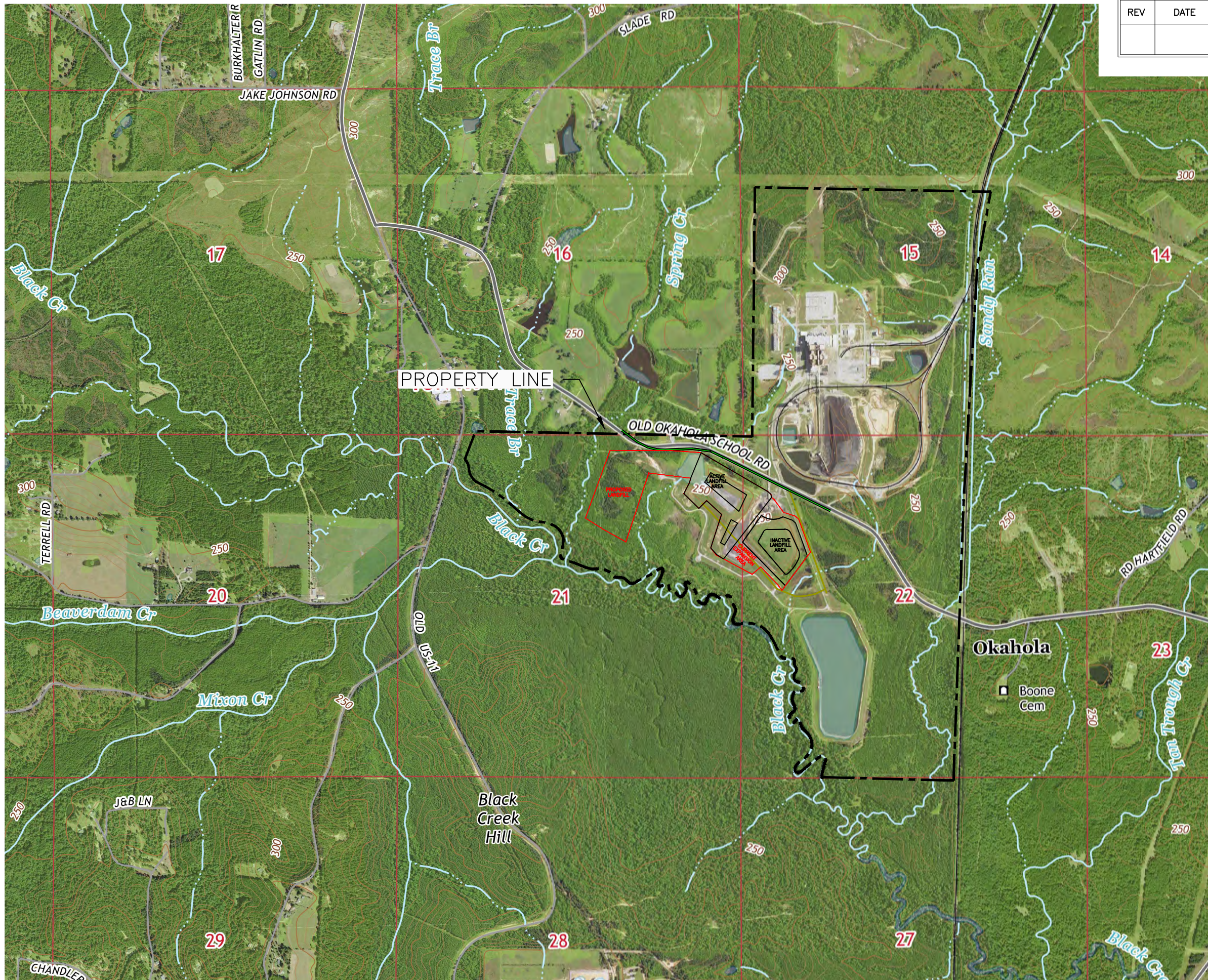
Chris T. Johnson, P.E., P.S.

Attachments

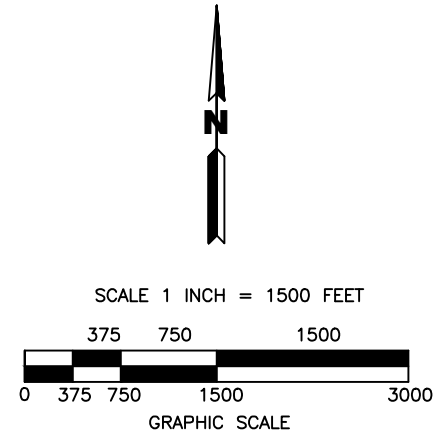
EMS Project No. SOU2-16-002



ATTACHMENT 1
FIGURES



| REVISIONS | | |
|-----------|------|---------|
| REV | DATE | REMARKS |
| | | |



LEGEND

- SMEPA PROPERTY BOUNDARY
- CAP BOUNDARY

ENVIRONMENTAL
MANAGEMENT SERVICES, INC.

P.O. BOX 15369
HATTIESBURG, MS 39404
601-544-3674 • 601-544-0504 (fax)

PREPARED FOR

SOUTH MISSISSIPPI
ELECTRIC
POWER ASSOCIATION

P.O. BOX 15849
HATTIESBURG, MS 39404-5849

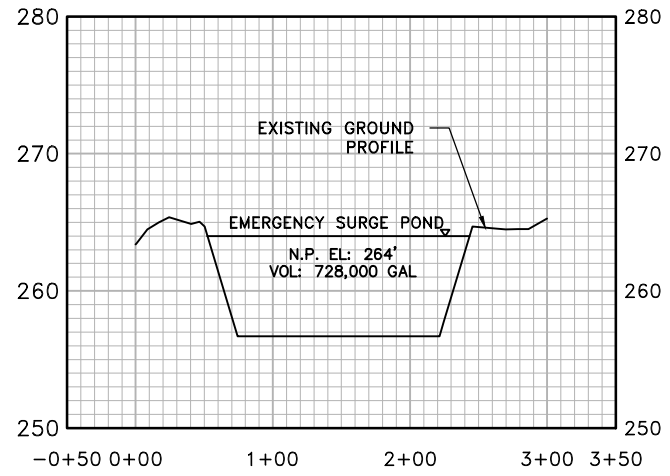
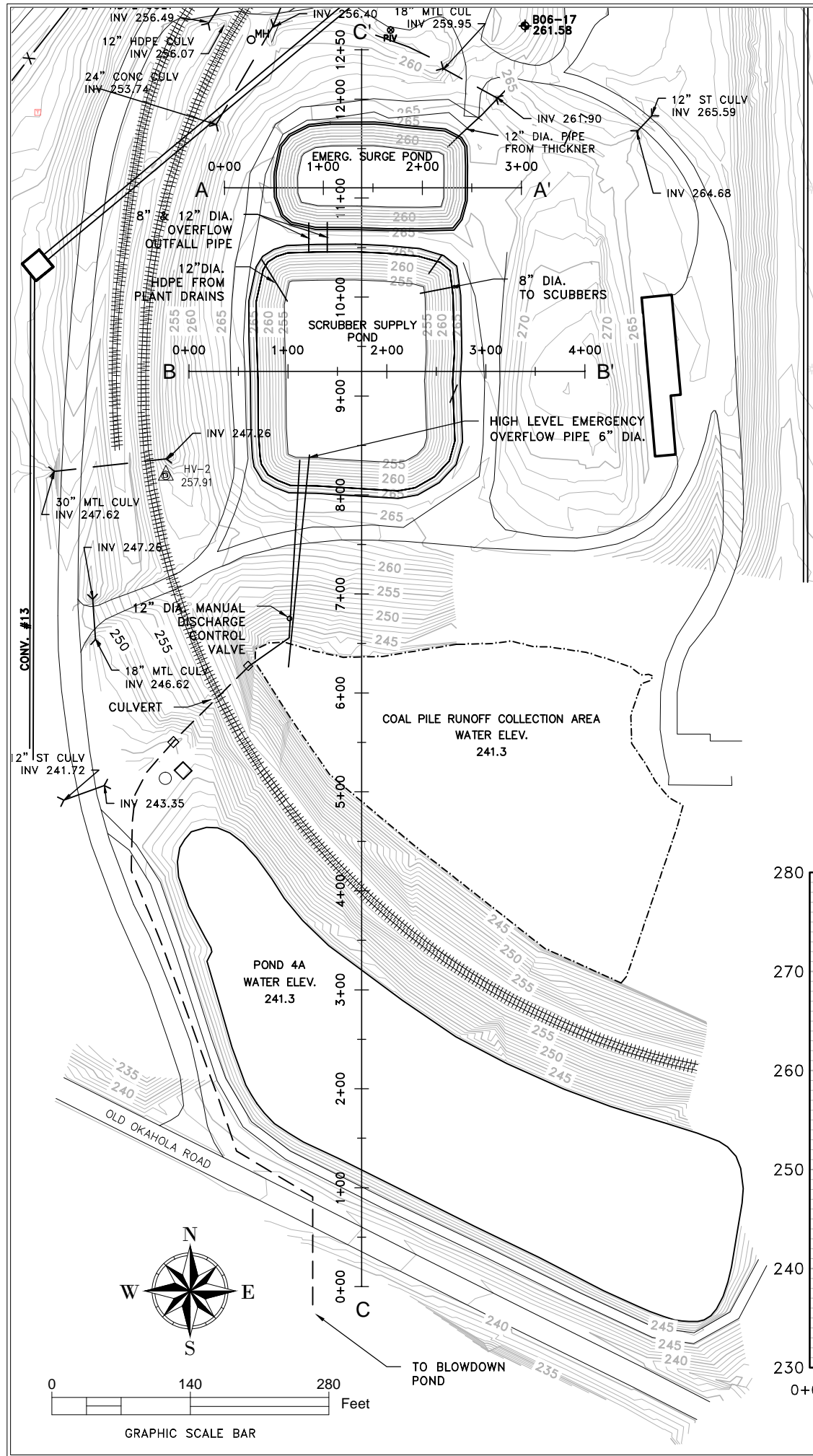
SITE LOCATION

R.D. MORROW SR. GENERATING STATION
PURVIS, MISSISSIPPI

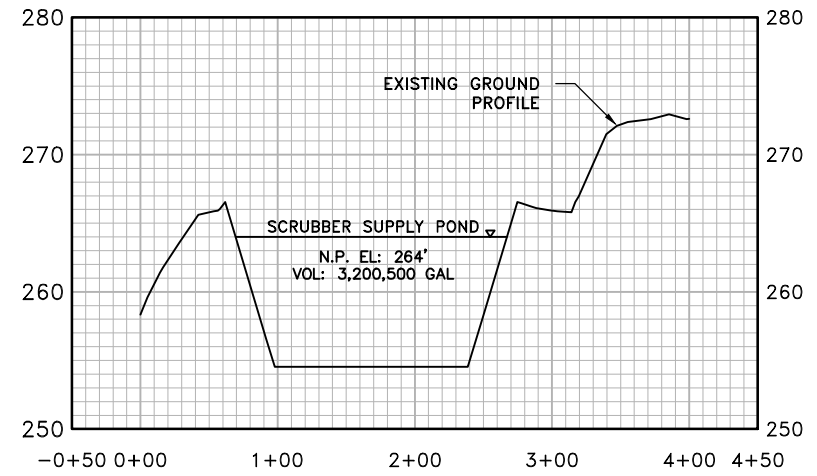
SHEET TITLE

| | |
|-------------|-------------|
| DATE | 10/11/2016 |
| SCALE | 1" = 1500' |
| DRAWN BY | PDM |
| PROJECT NO. | SOU2-16-002 |
| SHEET NO. | 1 |

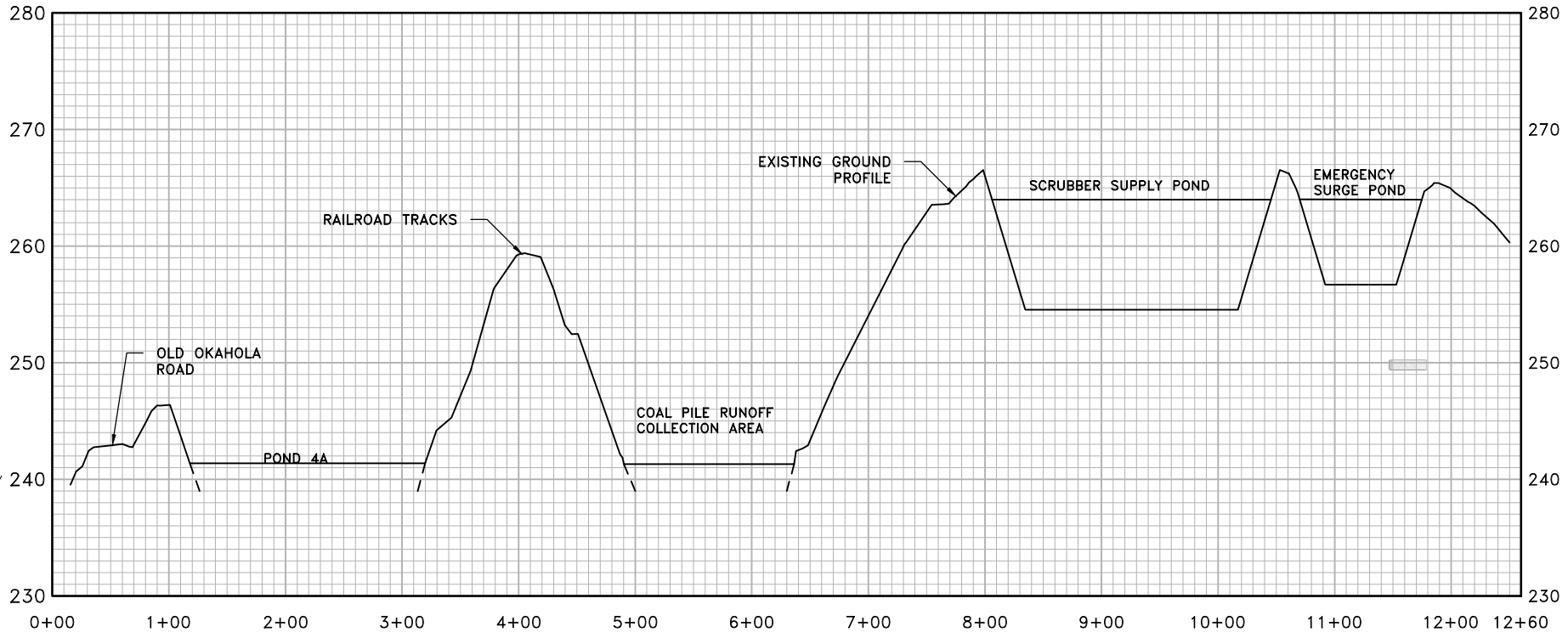
REFERENCE: 7.5 MIN. SERIES TOPOGRAPHIC MAP
PURVIS, MISSISSIPPI



SECTION A - A'



SECTION B - B'



SECTION C - C'

PREPARED FOR

CCR IMPOUNDMENT PLAN-PROFILE
R.D. MORROW SR. GENERATING STATION

SHEET TITLE

DATE
10-06-2016

SCALE
AS SHOWN

SHEET NO.
2

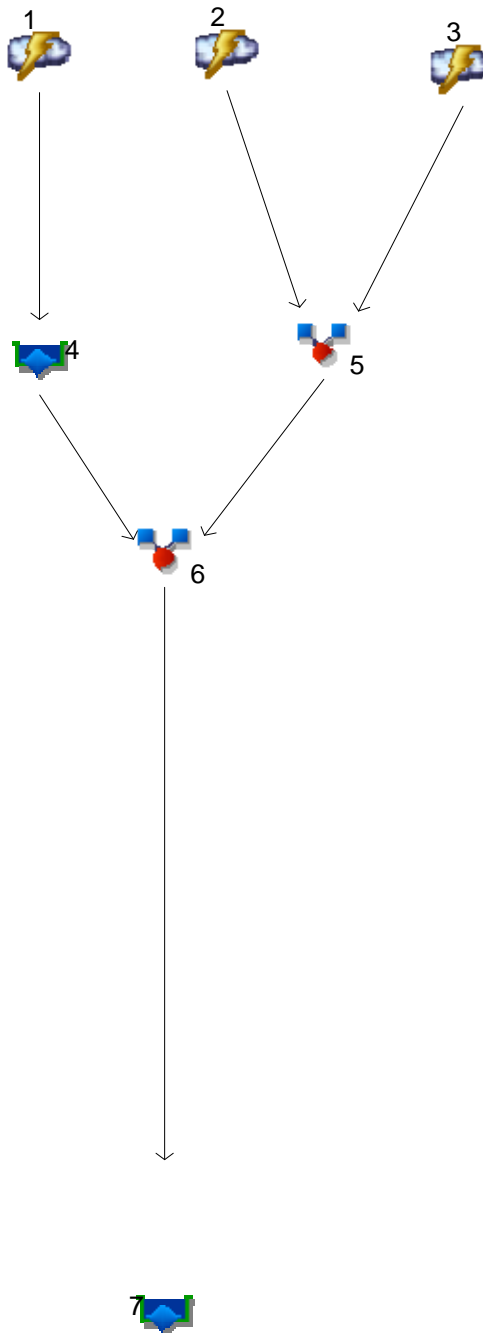
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SOU2-16-002

ATTACHMENT 2
HYDROLOGIC & HYDRAULIC
MODEL/RESULTS

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Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3



Legend

| Hyd. Origin | Description |
|-------------|------------------------------|
| 1 Rational | Surge Pond Basin |
| 2 Rational | Scrubber Supply Basin |
| 3 Rational | Plant Drains |
| 4 Reservoir | Route to Surge Pond |
| 5 Combine | Combined Flow to Supply Pond |
| 6 Combine | Total Flow to Supply Pond |
| 7 Reservoir | Scrubber Supply Pond |

Hydrograph Return Period Recap

Hydranow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

| Hyd. No. | Hydrograph type (origin) | Inflow hyd(s) | Peak Outflow (cfs) | | | | | | | | Hydrograph Description |
|----------|--------------------------|---------------|--------------------|-------|-------|-------|-------|-------|-------|--------|------------------------------|
| | | | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | |
| 1 | Rational | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 15.04 | Surge Pond Basin |
| 2 | Rational | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 30.90 | Scrubber Supply Basin |
| 3 | Rational | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 115.15 | Plant Drains |
| 4 | Reservoir | 1 | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 0.038 | Route to Surge Pond |
| 5 | Combine | 2, 3, | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 115.15 | Combined Flow to Supply Pond |
| 6 | Combine | 4, 5 | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 115.19 | Total Flow to Supply Pond |
| 7 | Reservoir | 6 | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 2.303 | Scrubber Supply Pond |

Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

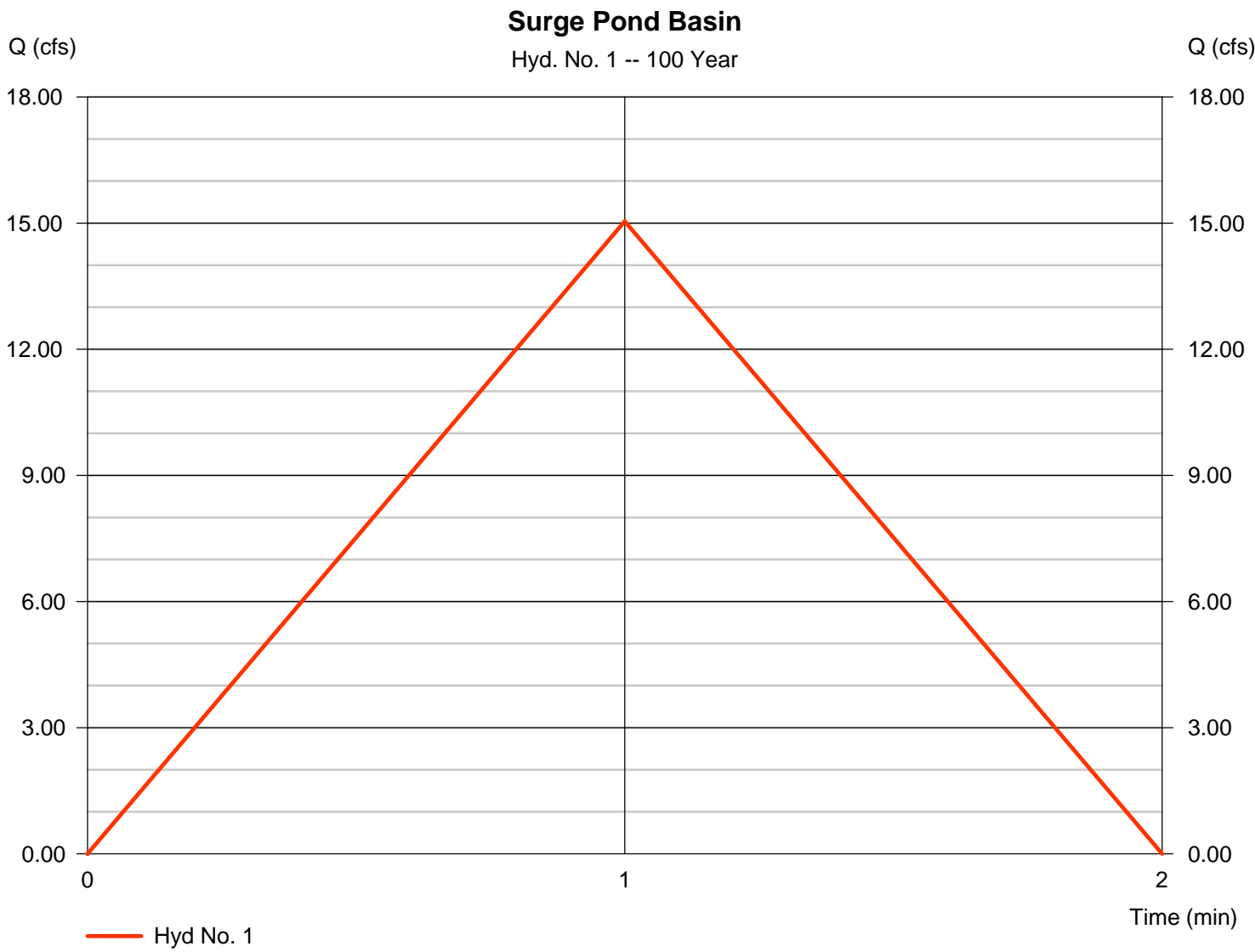
| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description | |
|---|--------------------------|-----------------|---------------------|--------------------|-------------------------|---------------|------------------------|---------------------------|------------------------------|--|
| 1 | Rational | 15.04 | 1 | 1 | 903 | ----- | ----- | ----- | Surge Pond Basin | |
| 2 | Rational | 30.90 | 1 | 1 | 1,854 | ----- | ----- | ----- | Scrubber Supply Basin | |
| 3 | Rational | 115.15 | 1 | 6 | 41,453 | ----- | ----- | ----- | Plant Drains | |
| 4 | Reservoir | 0.038 | 1 | 2 | 879 | 1 | 264.04 | 101,280 | Route to Surge Pond | |
| 5 | Combine | 115.15 | 1 | 6 | 43,307 | 2, 3, | ----- | ----- | Combined Flow to Supply Pond | |
| 6 | Combine | 115.19 | 1 | 6 | 44,186 | 4, 5 | ----- | ----- | Total Flow to Supply Pond | |
| 7 | Reservoir | 2.303 | 1 | 12 | 38,744 | 6 | 262.87 | 317,513 | Scrubber Supply Pond | |
| CCR Impoundments Final (10-12-2016).gpw | | | | | Return Period: 100 Year | | | Wednesday, 10 / 12 / 2016 | | |

Hydrograph Report

Hyd. No. 1

Surge Pond Basin

| | | | |
|-----------------|--------------------------------|------------------|-------------|
| Hydrograph type | = Rational | Peak discharge | = 15.04 cfs |
| Storm frequency | = 100 yrs | Time to peak | = 1 min |
| Time interval | = 1 min | Hyd. volume | = 903 cuft |
| Drainage area | = 0.740 ac | Runoff coeff. | = 0.99 |
| Intensity | = 20.533 in/hr | Tc by User | = 1.00 min |
| IDF Curve | = Hattiesburg Lamar IDF Curves | AB/Rec limb fact | = 1/1 |



Hydrograph Report

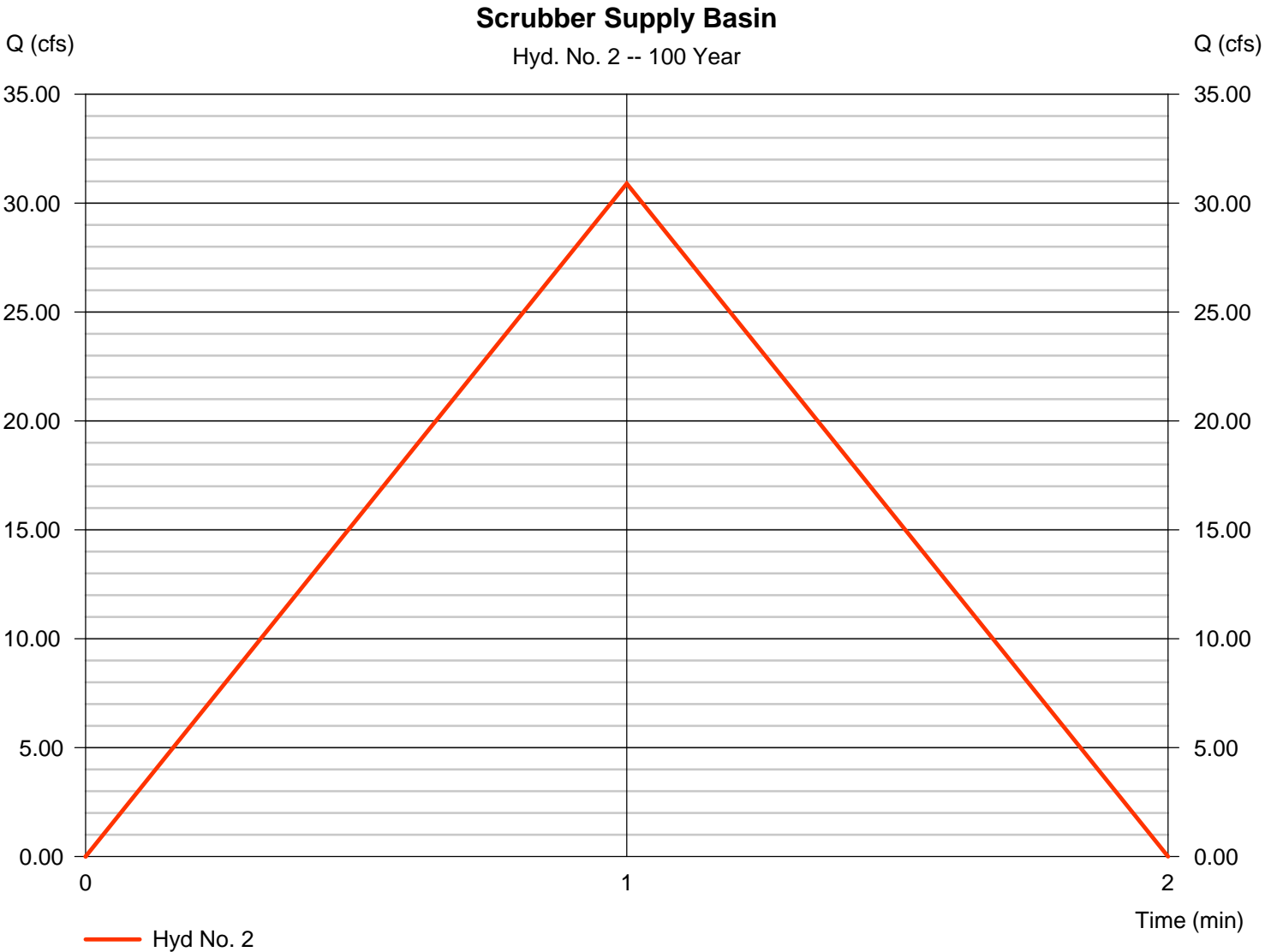
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Wednesday, 10 / 12 / 2016

Hyd. No. 2

Scrubber Supply Basin

| | | | |
|-----------------|--------------------------------|------------------|--------------|
| Hydrograph type | = Rational | Peak discharge | = 30.90 cfs |
| Storm frequency | = 100 yrs | Time to peak | = 1 min |
| Time interval | = 1 min | Hyd. volume | = 1,854 cuft |
| Drainage area | = 1.520 ac | Runoff coeff. | = 0.99 |
| Intensity | = 20.533 in/hr | Tc by User | = 1.00 min |
| IDF Curve | = Hattiesburg Lamar IDF Curves | AB/Rec limb fact | = 1/1 |



Hydrograph Report

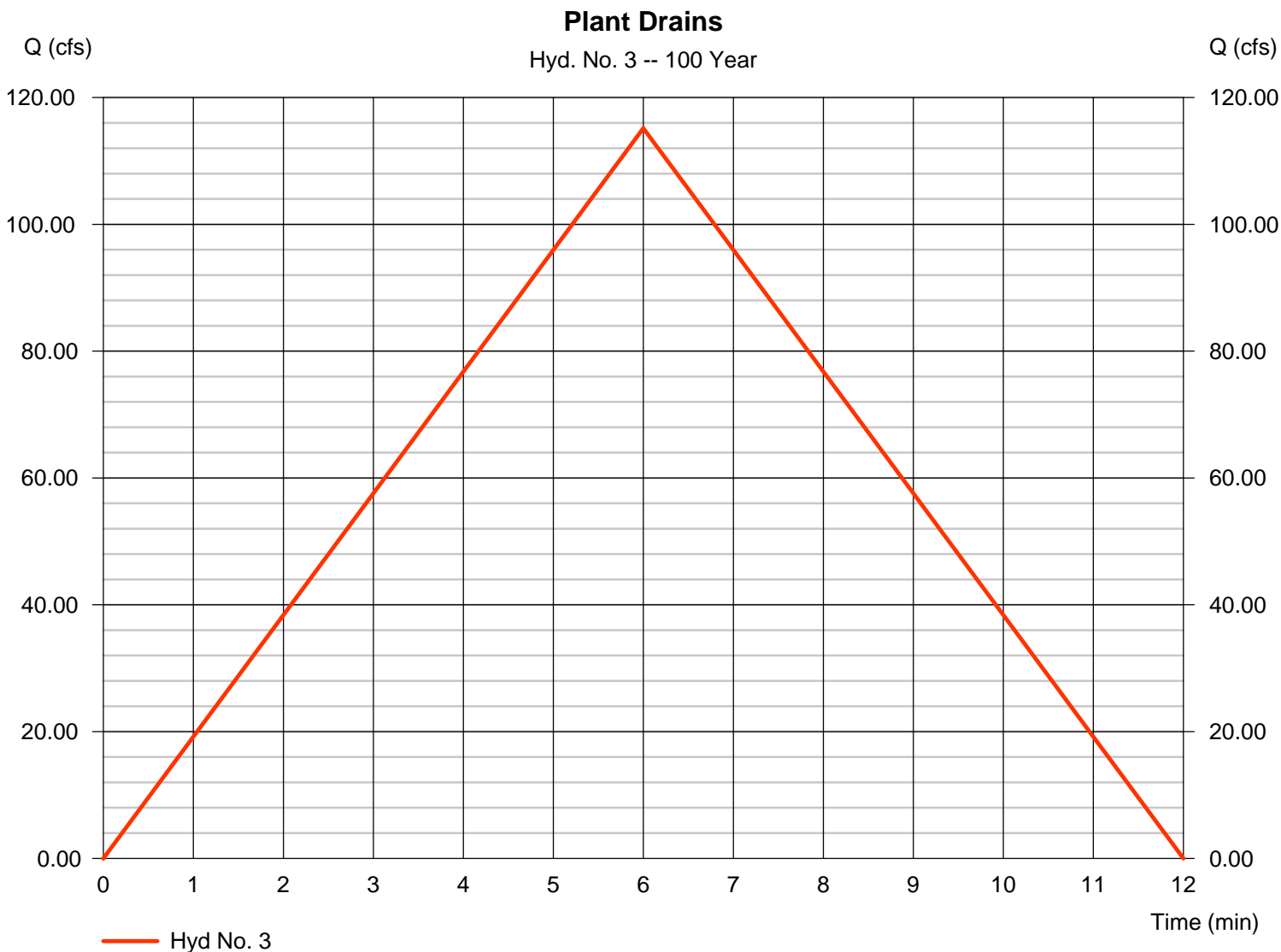
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Wednesday, 10 / 12 / 2016

Hyd. No. 3

Plant Drains

| | | | |
|-----------------|--------------------------------|------------------|---------------|
| Hydrograph type | = Rational | Peak discharge | = 115.15 cfs |
| Storm frequency | = 100 yrs | Time to peak | = 6 min |
| Time interval | = 1 min | Hyd. volume | = 41,453 cuft |
| Drainage area | = 10.000 ac | Runoff coeff. | = 0.9 |
| Intensity | = 12.794 in/hr | Tc by User | = 6.00 min |
| IDF Curve | = Hattiesburg Lamar IDF Curves | AB/Rec limb fact | = 1/1 |



Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

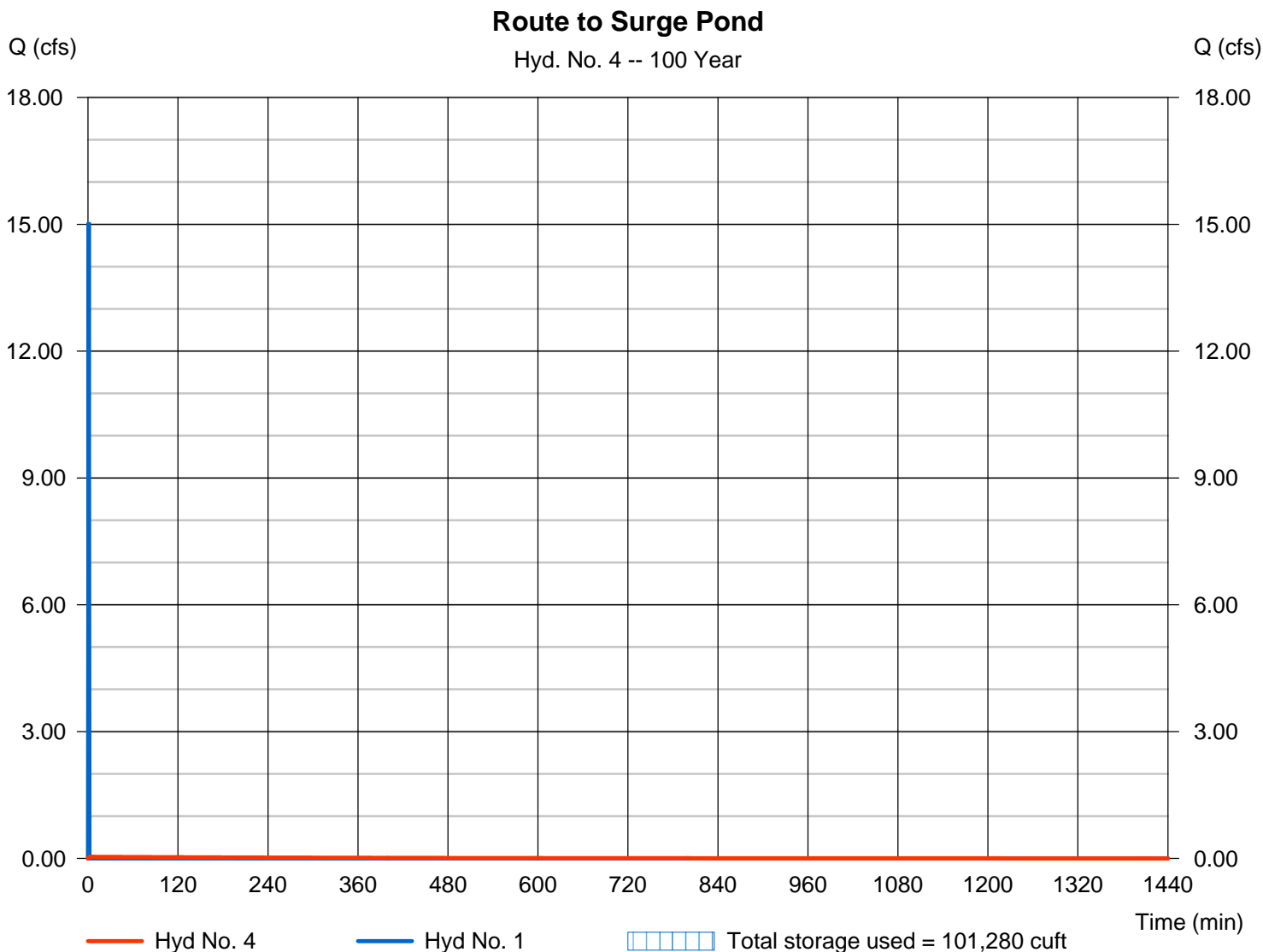
Wednesday, 10 / 12 / 2016

Hyd. No. 4

Route to Surge Pond

| | | | |
|-----------------|------------------------|----------------|----------------|
| Hydrograph type | = Reservoir | Peak discharge | = 0.038 cfs |
| Storm frequency | = 100 yrs | Time to peak | = 2 min |
| Time interval | = 1 min | Hyd. volume | = 879 cuft |
| Inflow hyd. No. | = 1 - Surge Pond Basin | Max. Elevation | = 264.04 ft |
| Reservoir name | = Em Surge Pond | Max. Storage | = 101,280 cuft |

Storage Indication method used. Wet pond routing start elevation = 264.00 ft.



Pond Report

Pond No. 1 - Em Surge Pond

Pond Data

Trapezoid -Bottom L x W = 150.0 x 62.0 ft, Side slope = 3.00:1, Bottom elev. = 257.00 ft, Depth = 10.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 257.00 | 9,300 | 0 | 0 |
| 1.00 | 258.00 | 10,608 | 9,948 | 9,948 |
| 2.00 | 259.00 | 11,988 | 11,292 | 21,240 |
| 3.00 | 260.00 | 13,440 | 12,708 | 33,948 |
| 4.00 | 261.00 | 14,964 | 14,196 | 48,144 |
| 5.00 | 262.00 | 16,560 | 15,756 | 63,900 |
| 6.00 | 263.00 | 18,228 | 17,388 | 81,288 |
| 7.00 | 264.00 | 19,968 | 19,092 | 100,380 |
| 8.00 | 265.00 | 21,780 | 20,868 | 121,248 |
| 9.00 | 266.00 | 23,664 | 22,716 | 143,964 |
| 10.00 | 267.00 | 25,620 | 24,636 | 168,600 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [PrfRsr] |
|-----------------|----------|------|------|----------|
| Rise (in) | = 12.00 | 0.00 | 0.00 | 0.00 |
| Span (in) | = 12.00 | 0.00 | 0.00 | 0.00 |
| No. Barrels | = 2 | 0 | 0 | 0 |
| Invert El. (ft) | = 264.00 | 0.00 | 0.00 | 0.00 |
| Length (ft) | = 26.00 | 0.00 | 0.00 | 0.00 |
| Slope (%) | = 1.00 | 0.00 | 0.00 | n/a |
| N-Value | = .013 | .013 | .013 | n/a |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 |
| Multi-Stage | = n/a | No | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|----------------|---------|---------------|------|------|
| Crest Len (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Crest El. (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Weir Type | = --- | --- | --- | --- |
| Multi-Stage | = No | No | No | No |
| Exfil.(in/hr) | = 0.000 | (by Wet area) | | |
| TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|------------|----------|----------|----------|----------|-----------|----------|-----------|
| 0.00 | 0 | 257.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.10 | 995 | 257.10 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.20 | 1,990 | 257.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.30 | 2,984 | 257.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.40 | 3,979 | 257.40 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.50 | 4,974 | 257.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.60 | 5,969 | 257.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.70 | 6,964 | 257.70 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.80 | 7,958 | 257.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.90 | 8,953 | 257.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.00 | 9,948 | 258.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.10 | 11,077 | 258.10 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.20 | 12,206 | 258.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.30 | 13,336 | 258.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.40 | 14,465 | 258.40 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.50 | 15,594 | 258.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.60 | 16,723 | 258.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.70 | 17,852 | 258.70 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.80 | 18,982 | 258.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.90 | 20,111 | 258.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.00 | 21,240 | 259.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.10 | 22,511 | 259.10 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.20 | 23,782 | 259.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.30 | 25,052 | 259.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.40 | 26,323 | 259.40 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.50 | 27,594 | 259.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.60 | 28,865 | 259.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.70 | 30,136 | 259.70 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.80 | 31,406 | 259.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.90 | 32,677 | 259.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.00 | 33,948 | 260.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.10 | 35,368 | 260.10 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |

Continues on next page...

Em Surge Pond

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 3.20 | 36,787 | 260.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.30 | 38,207 | 260.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.40 | 39,626 | 260.40 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.50 | 41,046 | 260.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.60 | 42,466 | 260.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.70 | 43,885 | 260.70 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.80 | 45,305 | 260.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.90 | 46,724 | 260.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.00 | 48,144 | 261.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.10 | 49,720 | 261.10 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.20 | 51,295 | 261.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.30 | 52,871 | 261.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.40 | 54,446 | 261.40 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.50 | 56,022 | 261.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.60 | 57,598 | 261.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.70 | 59,173 | 261.70 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.80 | 60,749 | 261.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.90 | 62,324 | 261.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.00 | 63,900 | 262.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.10 | 65,639 | 262.10 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.20 | 67,378 | 262.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.30 | 69,116 | 262.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.40 | 70,855 | 262.40 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.50 | 72,594 | 262.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.60 | 74,333 | 262.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.70 | 76,072 | 262.70 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.80 | 77,810 | 262.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.90 | 79,549 | 262.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.00 | 81,288 | 263.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.10 | 83,197 | 263.10 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.20 | 85,106 | 263.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.30 | 87,016 | 263.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.40 | 88,925 | 263.40 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.50 | 90,834 | 263.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.60 | 92,743 | 263.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.70 | 94,652 | 263.70 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.80 | 96,562 | 263.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.90 | 98,471 | 263.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.00 | 100,380 | 264.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.10 | 102,467 | 264.10 | 0.09 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.088 |
| 7.20 | 104,554 | 264.20 | 0.34 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.342 |
| 7.30 | 106,640 | 264.30 | 0.74 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.742 |
| 7.40 | 108,727 | 264.40 | 1.26 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 1.264 |
| 7.50 | 110,814 | 264.50 | 1.89 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 1.895 |
| 7.60 | 112,901 | 264.60 | 2.60 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 2.599 |
| 7.70 | 114,988 | 264.70 | 3.29 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 3.287 |
| 7.80 | 117,074 | 264.80 | 3.79 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 3.787 |
| 7.90 | 119,161 | 264.90 | 4.17 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.169 |
| 8.00 | 121,248 | 265.00 | 4.23 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.233 |
| 8.10 | 123,519 | 265.10 | 4.98 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.981 |
| 8.20 | 125,791 | 265.20 | 5.63 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 5.630 |
| 8.30 | 128,063 | 265.30 | 6.21 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.212 |
| 8.40 | 130,334 | 265.40 | 6.74 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.744 |
| 8.50 | 132,606 | 265.50 | 7.24 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.237 |
| 8.60 | 134,877 | 265.60 | 7.70 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.698 |
| 8.70 | 137,149 | 265.70 | 8.13 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 8.133 |
| 8.80 | 139,421 | 265.80 | 8.55 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 8.547 |
| 8.90 | 141,692 | 265.90 | 8.94 oc | --- | --- | --- | --- | --- | --- | --- | --- | --- | 8.941 |
| 9.00 | 143,964 | 266.00 | 9.26 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 9.262 |
| 9.10 | 146,427 | 266.10 | 9.57 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 9.566 |
| 9.20 | 148,891 | 266.20 | 9.86 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 9.860 |
| 9.30 | 151,355 | 266.30 | 10.15 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 10.15 |
| 9.40 | 153,818 | 266.40 | 10.42 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 10.42 |
| 9.50 | 156,282 | 266.50 | 10.69 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 10.69 |
| 9.60 | 158,745 | 266.60 | 10.96 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 10.96 |
| 9.70 | 161,209 | 266.70 | 11.22 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 11.22 |
| 9.80 | 163,673 | 266.80 | 11.47 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 11.47 |
| 9.90 | 166,136 | 266.90 | 11.72 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 11.72 |
| 10.00 | 168,600 | 267.00 | 11.96 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 11.96 |

...End

Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

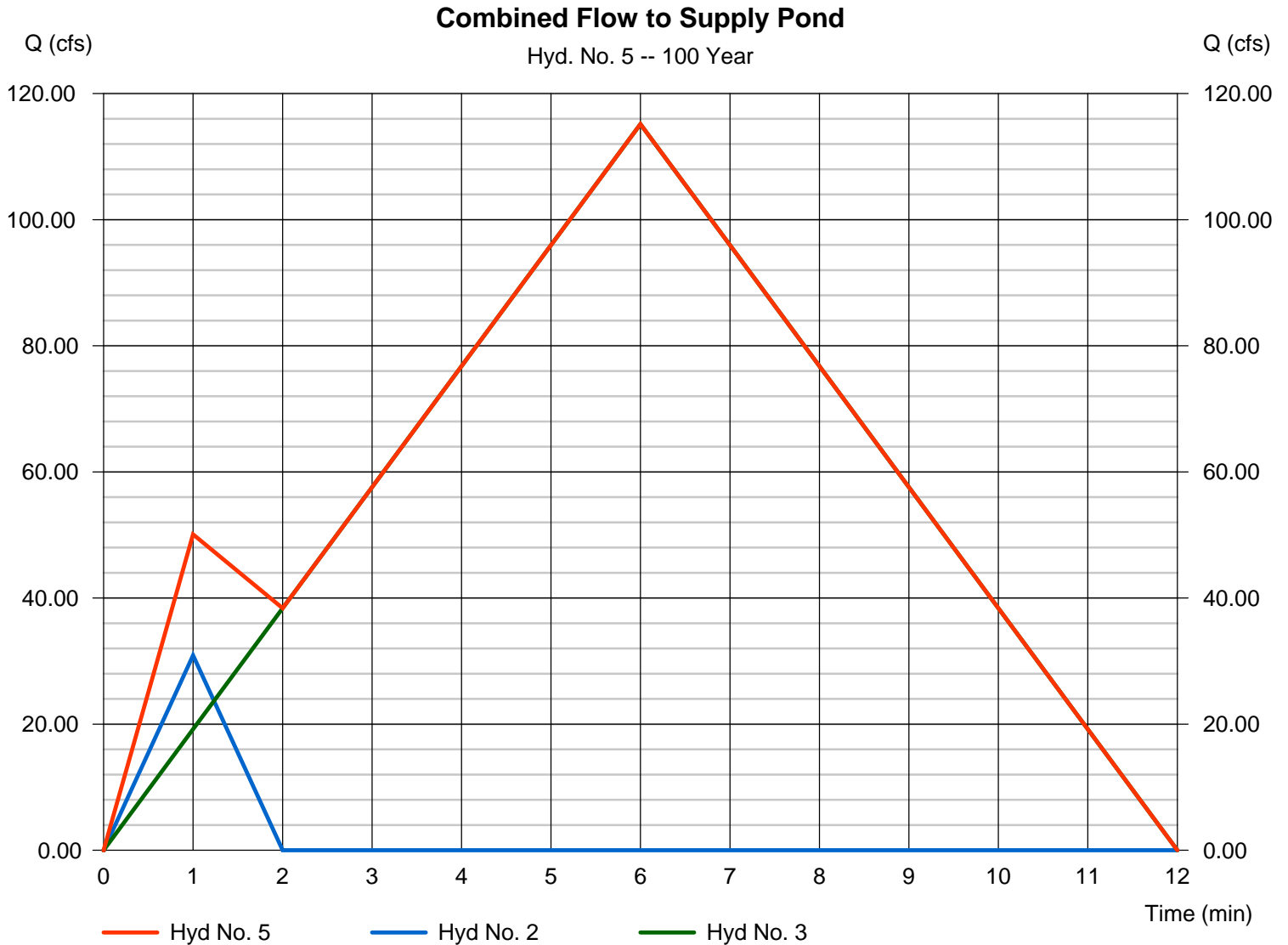
Wednesday, 10 / 12 / 2016

Hyd. No. 5

Combined Flow to Supply Pond

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 1 min
Inflow hyds. = 2, 3

Peak discharge = 115.15 cfs
Time to peak = 6 min
Hyd. volume = 43,307 cuft
Contrib. drain. area = 11.520 ac



Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Wednesday, 10 / 12 / 2016

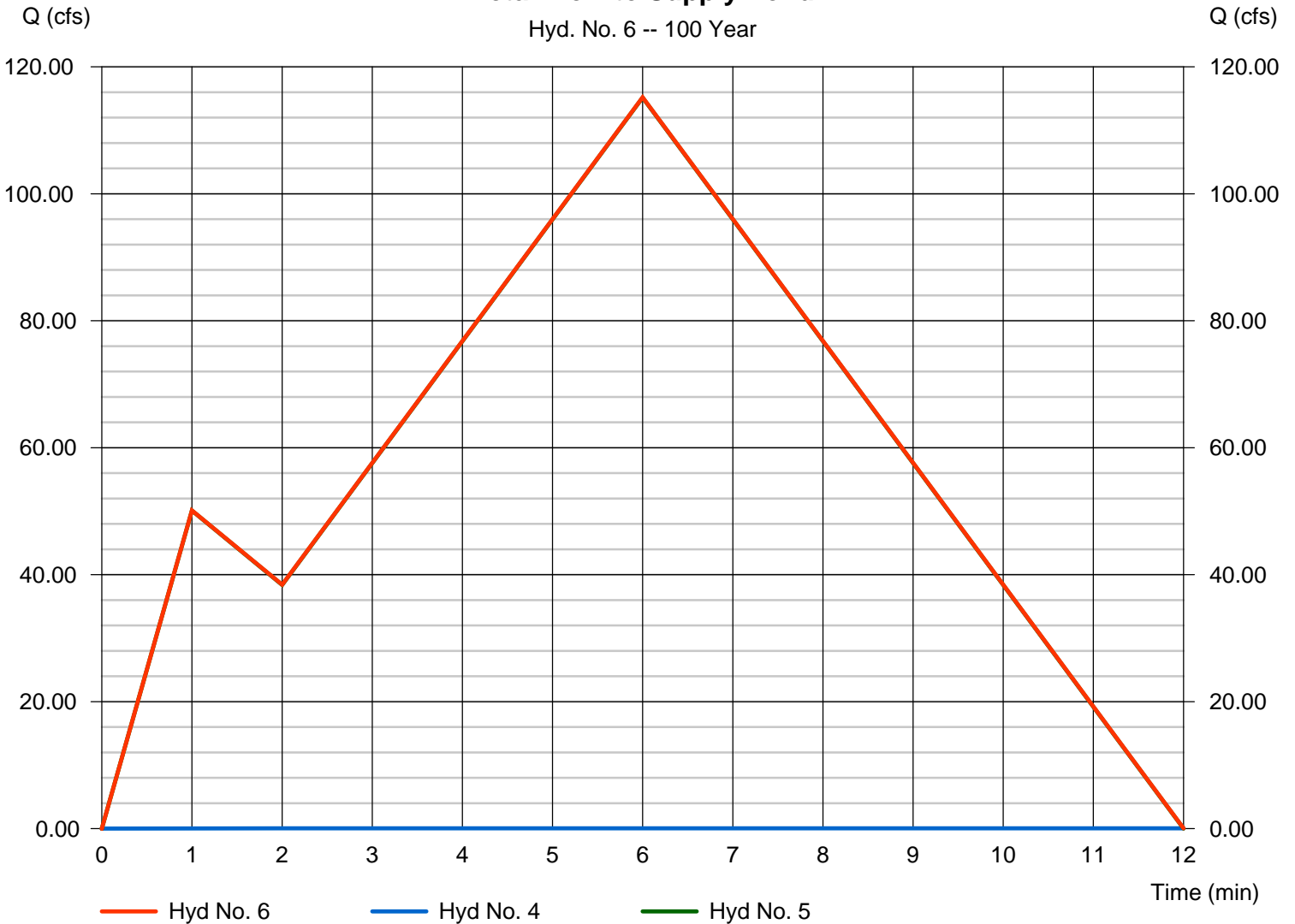
Hyd. No. 6

Total Flow to Supply Pond

| | | | |
|-----------------|-----------|----------------------|---------------|
| Hydrograph type | = Combine | Peak discharge | = 115.19 cfs |
| Storm frequency | = 100 yrs | Time to peak | = 6 min |
| Time interval | = 1 min | Hyd. volume | = 44,186 cuft |
| Inflow hyds. | = 4, 5 | Contrib. drain. area | = 0.000 ac |

Total Flow to Supply Pond

Hyd. No. 6 -- 100 Year



Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Wednesday, 10 / 12 / 2016

Hyd. No. 7

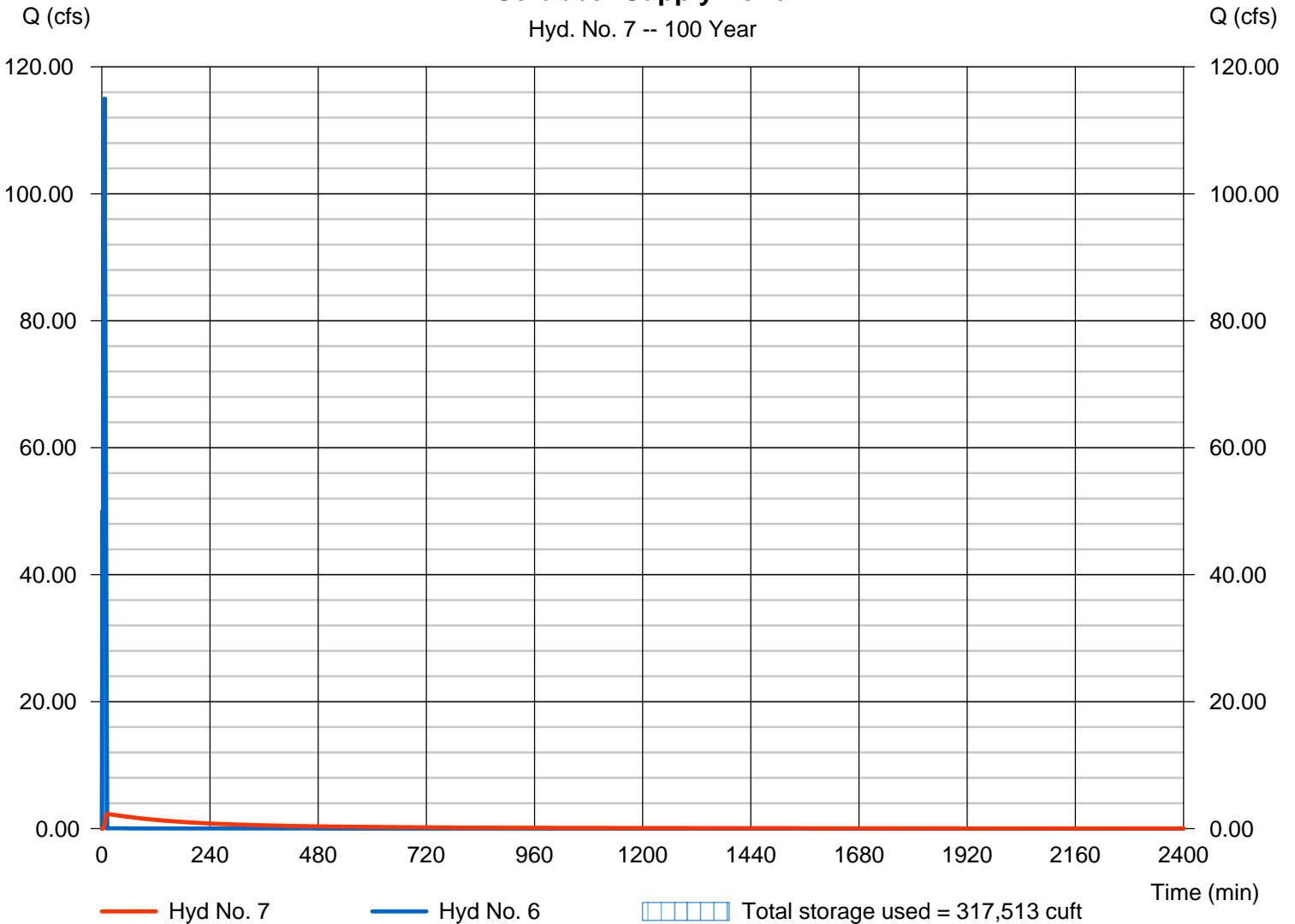
Scrubber Supply Pond

| | | | |
|-----------------|---------------------------------|----------------|----------------|
| Hydrograph type | = Reservoir | Peak discharge | = 2.303 cfs |
| Storm frequency | = 100 yrs | Time to peak | = 12 min |
| Time interval | = 1 min | Hyd. volume | = 38,744 cuft |
| Inflow hyd. No. | = 6 - Total Flow to Supply Pond | Max. Elevation | = 262.87 ft |
| Reservoir name | = Scrubber Supply Pond | Max. Storage | = 317,513 cuft |

Storage Indication method used. Wet pond routing start elevation = 261.93 ft.

Scrubber Supply Pond

Hyd. No. 7 -- 100 Year



Pond Report

Pond No. 2 - Scrubber Supply Pond

Pond Data

Trapezoid -Bottom L x W = 184.0 x 142.0 ft, Side slope = 3.00:1, Bottom elev. = 254.00 ft, Depth = 13.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 254.00 | 26,128 | 0 | 0 |
| 1.30 | 255.30 | 28,732 | 35,646 | 35,646 |
| 2.60 | 256.60 | 31,457 | 39,109 | 74,755 |
| 3.90 | 257.90 | 34,304 | 42,731 | 117,486 |
| 5.20 | 259.20 | 37,273 | 46,512 | 163,998 |
| 6.50 | 260.50 | 40,363 | 50,450 | 214,448 |
| 7.80 | 261.80 | 43,575 | 54,547 | 268,994 |
| 9.10 | 263.10 | 46,909 | 58,801 | 327,796 |
| 10.40 | 264.40 | 50,364 | 63,214 | 391,010 |
| 11.70 | 265.70 | 53,941 | 67,785 | 458,795 |
| 13.00 | 267.00 | 57,640 | 72,514 | 531,309 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [PrfRsr] |
|-----------------|----------|------|------|----------|
| Rise (in) | = 12.00 | 0.00 | 0.00 | 0.00 |
| Span (in) | = 12.00 | 0.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 0 | 0 | 0 |
| Invert El. (ft) | = 262.00 | 0.00 | 0.00 | 0.00 |
| Length (ft) | = 100.00 | 0.00 | 0.00 | 0.00 |
| Slope (%) | = 4.00 | 0.00 | 0.00 | n/a |
| N-Value | = .013 | .013 | .013 | n/a |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 |
| Multi-Stage | = n/a | No | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|----------------|---------|---------------|------|------|
| Crest Len (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Crest El. (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Weir Type | = --- | --- | --- | --- |
| Multi-Stage | = No | No | No | No |
| Exfil.(in/hr) | = 0.000 | (by Wet area) | | |
| TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|------------|----------|----------|----------|----------|-----------|----------|-----------|
| 0.00 | 0 | 254.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.13 | 3,565 | 254.13 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.26 | 7,129 | 254.26 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.39 | 10,694 | 254.39 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.52 | 14,258 | 254.52 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.65 | 17,823 | 254.65 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.78 | 21,387 | 254.78 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.91 | 24,952 | 254.91 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.04 | 28,516 | 255.04 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.17 | 32,081 | 255.17 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.30 | 35,646 | 255.30 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.43 | 39,557 | 255.43 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.56 | 43,467 | 255.56 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.69 | 47,378 | 255.69 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.82 | 51,289 | 255.82 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 1.95 | 55,200 | 255.95 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.08 | 59,111 | 256.08 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.21 | 63,022 | 256.21 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.34 | 66,933 | 256.34 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.47 | 70,844 | 256.47 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.60 | 74,755 | 256.60 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.73 | 79,028 | 256.73 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.86 | 83,301 | 256.86 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 2.99 | 87,574 | 256.99 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.12 | 91,848 | 257.12 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.25 | 96,121 | 257.25 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.38 | 100,394 | 257.38 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.51 | 104,667 | 257.51 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.64 | 108,940 | 257.64 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.77 | 113,213 | 257.77 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 3.90 | 117,486 | 257.90 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.03 | 122,138 | 258.03 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |

Continues on next page...

Scrubber Supply Pond

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 4.16 | 126,789 | 258.16 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.29 | 131,440 | 258.29 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.42 | 136,091 | 258.42 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.55 | 140,742 | 258.55 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.68 | 145,393 | 258.68 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.81 | 150,045 | 258.81 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 4.94 | 154,696 | 258.94 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.07 | 159,347 | 259.07 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.20 | 163,998 | 259.20 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.33 | 169,043 | 259.33 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.46 | 174,088 | 259.46 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.59 | 179,133 | 259.59 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.72 | 184,178 | 259.72 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.85 | 189,223 | 259.85 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 5.98 | 194,268 | 259.98 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.11 | 199,313 | 260.11 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.24 | 204,358 | 260.24 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.37 | 209,403 | 260.37 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.50 | 214,448 | 260.50 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.63 | 219,493 | 260.63 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.76 | 225,537 | 260.76 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 6.89 | 230,582 | 260.89 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.02 | 236,627 | 261.02 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.15 | 241,672 | 261.15 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.28 | 247,717 | 261.28 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.41 | 252,762 | 261.41 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.54 | 258,807 | 261.54 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.67 | 263,852 | 261.67 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.80 | 268,897 | 261.80 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 7.93 | 274,942 | 261.93 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 8.06 | 280,987 | 262.06 | 0.02 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.016 |
| 8.19 | 286,635 | 262.19 | 0.15 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.155 |
| 8.32 | 292,515 | 262.32 | 0.42 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.418 |
| 8.45 | 298,395 | 262.45 | 0.78 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 0.784 |
| 8.58 | 304,275 | 262.58 | 1.23 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 1.226 |
| 8.71 | 310,155 | 262.71 | 1.71 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 1.711 |
| 8.84 | 316,035 | 262.84 | 2.20 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 2.199 |
| 8.97 | 321,916 | 262.97 | 2.61 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 2.611 |
| 9.10 | 327,796 | 263.10 | 2.93 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 2.929 |
| 9.23 | 334,117 | 263.23 | 3.23 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 3.231 |
| 9.36 | 340,438 | 263.36 | 3.51 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 3.507 |
| 9.49 | 346,760 | 263.49 | 3.76 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 3.762 |
| 9.62 | 353,081 | 263.62 | 4.00 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.002 |
| 9.75 | 359,403 | 263.75 | 4.23 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.228 |
| 9.88 | 365,724 | 263.88 | 4.44 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.442 |
| 10.01 | 372,045 | 264.01 | 4.65 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.646 |
| 10.14 | 378,367 | 264.14 | 4.84 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 4.842 |
| 10.27 | 384,688 | 264.27 | 5.03 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 5.031 |
| 10.40 | 391,010 | 264.40 | 5.21 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 5.212 |
| 10.53 | 397,788 | 264.53 | 5.39 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 5.387 |
| 10.66 | 404,567 | 264.66 | 5.56 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 5.557 |
| 10.79 | 411,345 | 264.79 | 5.72 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 5.722 |
| 10.92 | 418,124 | 264.92 | 5.88 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 5.882 |
| 11.05 | 424,902 | 265.05 | 6.04 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.038 |
| 11.18 | 431,681 | 265.18 | 6.19 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.190 |
| 11.31 | 438,459 | 265.31 | 6.34 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.338 |
| 11.44 | 445,238 | 265.44 | 6.48 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.483 |
| 11.57 | 452,017 | 265.57 | 6.63 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.625 |
| 11.70 | 458,795 | 265.70 | 6.76 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.764 |
| 11.83 | 466,046 | 265.83 | 6.90 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 6.900 |
| 11.96 | 473,298 | 265.96 | 7.03 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.033 |
| 12.09 | 480,549 | 266.09 | 7.16 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.164 |
| 12.22 | 487,801 | 266.22 | 7.29 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.293 |
| 12.35 | 495,052 | 266.35 | 7.42 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.419 |
| 12.48 | 502,304 | 266.48 | 7.54 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.544 |
| 12.61 | 509,555 | 266.61 | 7.67 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.666 |
| 12.74 | 516,806 | 266.74 | 7.79 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.786 |
| 12.87 | 524,058 | 266.87 | 7.90 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.904 |
| 13.00 | 531,309 | 267.00 | 8.02 ic | --- | --- | --- | --- | --- | --- | --- | --- | --- | 8.021 |

...End

Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Wednesday, 10 / 12 / 2016

| Return Period (Yrs) | Intensity-Duration-Frequency Equation Coefficients (FHA) | | | |
|---------------------|--|---------|--------|-------|
| | B | D | E | (N/A) |
| 1 | 30.4792 | 5.5000 | 0.6739 | ----- |
| 2 | 35.6490 | 5.7000 | 0.6778 | ----- |
| 3 | 68.4227 | 10.8000 | 0.8016 | ----- |
| 5 | 40.9922 | 5.5000 | 0.6641 | ----- |
| 10 | 43.7048 | 5.1000 | 0.6472 | ----- |
| 25 | 44.3576 | 4.2000 | 0.6129 | ----- |
| 50 | 44.6596 | 3.7000 | 0.5888 | ----- |
| 100 | 42.3463 | 2.7000 | 0.5533 | ----- |

File name: Hattiesburg Lamar IDF Curves.IDF

$$\text{Intensity} = B / (T_c + D)^E$$

| Return Period (Yrs) | Intensity Values (in/hr) | | | | | | | | | | | |
|---------------------|--------------------------|-------|------|------|------|------|------|------|------|------|------|------|
| | 5 min | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 |
| 1 | 6.25 | 4.81 | 3.98 | 3.44 | 3.05 | 2.75 | 2.52 | 2.33 | 2.17 | 2.03 | 1.92 | 1.82 |
| 2 | 7.15 | 5.51 | 4.57 | 3.95 | 3.50 | 3.16 | 2.89 | 2.67 | 2.49 | 2.34 | 2.21 | 2.09 |
| 3 | 7.49 | 6.01 | 5.05 | 4.38 | 3.89 | 3.50 | 3.19 | 2.94 | 2.72 | 2.54 | 2.39 | 2.25 |
| 5 | 8.60 | 6.64 | 5.52 | 4.77 | 4.24 | 3.83 | 3.51 | 3.25 | 3.03 | 2.85 | 2.69 | 2.55 |
| 10 | 9.79 | 7.54 | 6.27 | 5.43 | 4.83 | 4.37 | 4.01 | 3.72 | 3.47 | 3.26 | 3.09 | 2.93 |
| 25 | 11.38 | 8.72 | 7.25 | 6.29 | 5.61 | 5.09 | 4.68 | 4.35 | 4.07 | 3.84 | 3.64 | 3.46 |
| 50 | 12.50 | 9.56 | 7.96 | 6.93 | 6.19 | 5.63 | 5.19 | 4.83 | 4.53 | 4.28 | 4.06 | 3.87 |
| 100 | 13.69 | 10.38 | 8.64 | 7.53 | 6.74 | 6.15 | 5.68 | 5.31 | 4.99 | 4.72 | 4.49 | 4.29 |

T_c = time in minutes. Values may exceed 60.

Finance Support\20 Hydrologic & Hydraulic Capacity Requirments\Inflow Control Plan\Lamar Co Precipitation Curves.pcp

| Storm Distribution | Rainfall Precipitation Table (in) | | | | | | | |
|--------------------|-----------------------------------|------|------|------|-------|-------|-------|--------|
| | 1-yr | 2-yr | 3-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr |
| SCS 24-hour | 0.00 | 4.86 | 0.00 | 3.30 | 7.05 | 8.55 | 6.80 | 11.10 |
| SCS 6-Hr | 0.00 | 3.50 | 0.00 | 0.00 | 5.04 | 6.11 | 0.00 | 7.95 |
| Huff-1st | 0.00 | 1.55 | 0.00 | 2.75 | 4.00 | 5.38 | 6.50 | 8.00 |
| Huff-2nd | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Huff-3rd | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Huff-4th | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Huff-Indy | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Custom | 0.00 | 1.75 | 0.00 | 2.80 | 3.90 | 5.25 | 6.00 | 7.10 |